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Chapter-4

## GEOMETRIC DESIGNING PARAMETERS AND ALIGNMENT DESCRIPTION

### 4.1 GENERAL

This chapter deals with geometrical standards adopted for horizontal and vertical alignments, route description, etc. The proposed corridors under Nagpur Metro Rail Project network will consist of Standard Gauge (SG) lines. For underground corridors, track centres are governed by spacing of tunnels and box design.

The geometrical design norms are based on international practices adopted for similar metro systems with standard gauge on the assumption that the maximum permissible speed on the section is limited to 80 kmph . Planning for any higher speed is not desirable as the average inter-station distance is about 1.30 km and trains will not be able to achieve higher speed.

The elevated tracks will be carried on box-shaped elevated decking supported by single circular piers, generally spaced at $25-\mathrm{m}$ centres and located on the median of the road. The horizontal alignment and vertical alignment are, therefore, dictated to a large extent by the geometry of the road and ground levels followed by the alignment.

The underground tracks will be carried in separate tunnels to be drilled by Tunnel Boring Machine. Stations will, however, be constructed by cut and cover method.

### 4.2 GEOMETRIC DESIGN PARAMETERS

The design parameters related to the Metro system described herewith have been worked out based on a detailed evaluation, experience and internationally accepted practices. Various alternatives were considered for most of these parameters but the best-suited ones have been adopted for the system as a whole.

### 4.2.1 Horizontal Alignment

As far as possible, the alignment follows the existing roads. This leads to introduction of horizontal curves. On consideration of desirable maximum cant of 110 mm and cant
deficiency of 85 mm on Metro tracks, the safe speed on curves of radii of 400 m or more is $80 \mathrm{~km} / \mathrm{h}$. On elevated sections minimum radius of 160 m has been used at one location having speed potential upto $40 \mathrm{~km} / \mathrm{h}$. However in underground section desirable minimum radius of curve shall be 300 m for ease of working of Tunnel Boring Machine (TBM). However in exceptional situation on this project, curves of 200 m radius (safe speed of $55 \mathrm{~km} / \mathrm{h}$ ) have been adopted where New Austrian Tunneling Machine (NATM) shall be used.

For maximum permissible speed on curve with various radii, Table 4.1 may be referred.
Horizontal Curves

| Description | Underground <br> Section | Elevated <br> Section |
| :--- | :---: | :---: |
| Desirable Minimum radius | 300 m | 200 m |
| Absolute minimum radius | 200 m (only c/c) | 120 m |
| Minimum curve radius at stations | 1000 m | 1000 m |
| Maximum permissible cant (Ca) | 125 mm | 125 mm |
| Maximum desirable cant | 110 mm | 110 mm |
| Maximum cant deficiency (Cd) | 85 mm | 85 mm |

### 4.2.2 Transition Curves

It is necessary to provide transition curves at both ends of the circular curves for smooth riding on the curves and to counter act centrifugal force. Due to change in gradients at various locations in the corridor, it is necessary to provide frequent vertical curves along the alignment. In case of ballast less track, it is desirable that the vertical curves and transition curves of horizontal curves do not overlap. These constraints may lead to reduced lengths of transition curves at certain locations. The transition curves have certain minimum parameters:

- Length of Transitions of Horizontal curves (m)

Minimum : 0.44 times actual cant or cant deficiency (in mm ), whichever is higher.
Desirable : 0.72 times actual cant or cant deficiency, (in mm ), whichever is higher.

- Overlap between transition curves and vertical curves not allowed.
- Minimum straight between two Transition curves (in case of reverse curves): either 25 m or Nil.
- Minimum straight between two Transition curves (in case of same flexure curves): either 25 m or both curves should be converted in to the compound curve by introducing single transition between the two circulars.
- Minimum curve length between two transition curves: 25 m


### 4.2.3 Vertical Alignment and Track Centre

## (a) Elevated Sections

The viaducts carrying the tracks will have a vertical clearance of minimum 5.5 m above road level. For meeting this requirement with the 'Box' shaped pre-stressed concrete girders, the rail level will be about 9.8 m above the road level. However, at stations which are located above central median, the rail level will be 13.5 m above the road level with concourse at mezzanine. These levels will, however, vary marginally depending upon where the stations are located.

The track center on the elevated section is kept as 4.1 m uniform throughout the corridor to standardize the superstructure, except at few locations, wherever scissors crossovers are planned, it is kept 4.5 meter.

## (b) Underground sections

Rail level at midsection in tunneling portion shall be kept at least 12.0 m below the ground level. At stations, the desirable depth of rail below ground level is 13.5 m , so that station concourse can be located above the platforms.

Track center in underground sections are follows:
Sections where stations are to be constructed
by cut \& cover and running section by TBM to
Accommodate 12 m wide platform : 15.05 m (for
lesser width of platform, track center to be reduced. )
Sections where stations are to be constructed
by NATM and running section by TBM to facilitate
Construction of stations
: 22.00 m
Sections where stations as well as running section
both are to be constructed by cut and cover method : 4.50 m
(c) Gradients

Normally the stations shall be on level stretch. In limited cases, station may be on a grade of $0.1 \%$. Between stations, generally the grades may not be steeper than 3.0 \%. However, where existing road gradients are steeper than 2 \%, or for Switch Over Ramps gradient up to 4\% (compensated) can be provided in short stretches on the main line.
(d) Vertical Curves

Vertical curves are to be provided when change in gradient exceeds $0.4 \%$. However, it is recommended to provide vertical curves at every change of gradient.
(e) Radius of vertical curves:

| - On main line (desirable) | $:$ | 2500 m |
| :--- | :--- | :--- |
| (Absolute minimum) | $:$ | 1500 m |
| - Other Locations | $:$ | 1500 m |
| - Minimum length of vertical curve | $:$ | 20 m |

### 4.2.4 Design Speed

The maximum sectional speed will be $85 \mathrm{~km} / \mathrm{h}$. However, the applied cant, and length of transition will be decided in relation to normal speeds at various locations, as determined by simulation studies of alignment, vertical profile and station locations. Computerized train simulation studies need to be conducted with proposed gradients at the time of detailed design stage. This is with the objective of keeping down the wear on rails on curves to the minimum.

Table 4.1: Cant, Permitted Speed \& Minimum Transition Length for Curves

| RADIUS | CANT | MAXIMUM <br> PERMISSIBLE <br> SPEED | MINIMUM DISTANCE BETWEEN <br> ADJACENT TRACKS |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | UNDERGROUND | ELEVATED AND <br> AT-GRADE |  |
| meters | mm | kmph | mm | Mm |
| 3000 | 15 | 80 | 3500 | 3650 |
| 2800 | 15 | 80 | 3500 | 3650 |
| 2400 | 20 | 80 | 3500 | 3650 |
| 2000 | 20 | 80 | 3500 | 3650 |
| 1600 | 25 | 80 | 3500 | 3650 |
| 1500 | 30 | 80 | 3500 | 3650 |
| 1200 | 35 | 80 | 3500 | 3650 |
| 1000 | 45 | 80 | 3500 | 3700 |
| 800 | 55 | 80 | 3550 | 3700 |
| 600 | 70 | 80 | 3550 | 3750 |
| 500 | 85 | 80 | 3600 | 3750 |
| 450 | 95 | 80 | 3600 | 3800 |
| 400 | 105 | 80 | 3650 | 3800 |
| 350 | 110 | 75 | 3650 | 3800 |
| 300 | 110 | 70 | 3700 | 3850 |
| 200 | 110 | 55 | 3800 | 3950 |
| $150^{*}$ | 110 | 45 | 4000 | 4050 |
| $150^{*}$ | 0 | 30 | 4000 | 4050 |
| $120^{*}$ | 110 | 40 | 4000 | 4150 |
| $120^{*}$ | 0 | 25 | 4000 | 4150 |
| $100^{*}$ | 110 | 40 |  |  |

Notes: (a) The track spacing is without any column/structure between two tracks and is with equal cant for both outer and inner tracks.
(b) Track spacing shown is not applicable to stations which should be calculated depending on specific requirement.
(c) Figures for any intermediate radius of curvature may be obtained by interpolating between two adjacent radii. For higher radii, values may be extrapolated.

### 4.2.5 Station Locations

Stations have been located so as to serve major passenger destinations and to enable
convenient integration with other modes of transport. However effort has also been made to propose station locations, such that inter station distances are as uniform as possible. The average spacing of stations is close to 1.2 km .

### 4.3 TRACK STRUCTURE

Track on Metro Systems is subjected to intensive usage with very little time for day-today maintenance. Thus it is imperative that the track structure selected for Metro Systems should be long lasting and should require minimum or no maintenance and at the same time, ensure highest level of safety, reliability and comfort, with minimum noise and vibrations. The track structure has been proposed keeping the above philosophy in view.
Two types of track structures are proposed for the corridors under Nagpur Metro Rail Project network. The normal ballasted track in Depot (except inside the Workshops, inspection lines and washing plant lines). The ballastless track is recommended on Viaducts and inside tunnels as the regular cleaning and replacement of ballast at such locations will not be possible.
For the depots, ballasted track is recommended as ballastless track on formation is not suitable due to settlement of formations. Ballastless track in depot is required inside the workshop, on inspection lines and washing plant lines.
From considerations of maintainability, riding comfort and also to contain vibrations and noise levels, the complete track is proposed to be joint-less and for this purpose even the turnouts will have to be incorporated in LWR/CWR.
The track will be laid with 1 in 20 canted rails and the wheel profile of Rolling Stock should be compatible with the rail cant and rail profile.

### 4.4 RAIL SECTION

Keeping in view the proposed axle load and the practices followed abroad, it is proposed to adopt UIC-60 ( $60 \mathrm{~kg} . / \mathrm{m}$ ) rail section. Since on main lines, sharp curves and steep gradients would be present, the grade of rail on main lines should be 1080 Head Hardened as per IRS-T-12-2009. As these rails are not manufactured in India at present, these are to be imported. For the Depot lines, the rails of grade 880 are recommended, which are available indigenously.

### 4.5 BALLASTLESS TRACK ON MAIN LINES

On the viaducts, it is proposed to adopt plinth type ballastless track structure with RCC derailment guards integrated with the plinths. Further, it is proposed to adopt fastening system complying to performance criteria laid down by Indian Railways on ballastless track structures, with a base-plate spacing of 60 cm . on viaducts.

In the underground sections, similar track structure with a base plate spacing of 70 cm is proposed on slab after $1^{\text {st }}$ stage concrete.

### 4.6 BALLASTLESS/BALLASTED TRACK IN DEPOT

The ballastless track in Depot may be of the following types:

- Supported on steel pedestal for inspection lines.
- Embedded rail type inside the Workshop.
- Plinth type for Washing line.
- $\quad$ Track is to be laid on PRC sleepers with sleeper spacing of 65 cm . All the rails are to be converted into rail panels by doing flash butt/Thermit welding.


### 4.7 TURNOUTS

All turn-outs/crossovers on the main lines and other running lines shall be as under:

Table 4.2: Turn-Outs

| S. No. | Description | Turn out Type |
| :--- | :--- | :---: |
| 01 | Main Line | 1 in 9 |
| 02 | Depot/Yard Lines | 1 in 7 |

### 4.8 BUFFER STOPS

On main lines and Depot lines, friction buffer stops with mechanical impact absorption (non-hydraulic type) will be provided. In elevated portion, the spans on which friction buffer stops are to be installed will be designed for an additional longitudinal force, which is likely to be transmitted in case of Rolling Stock hits, the friction Buffer Stops.

### 4.9 RAIL STRUCTURE INTERACTION

For continuing LWR/CWR on Viaducts, the elevated structures will be adequately designed for the additional longitudinal forces likely to be transmitted as a result of Rail-Structure interaction. Rail structure interaction study will determine the need and locations of Rail Expansion Joints (REJ) required to be provided.

### 4.10 ROUTE ALIGNMENT

Two Corridors have been identified for implementation in phase I of Nagpur Metro Rail Project network as per details given underneath:-
i) Automotive Square to KHAPRI
ii) Prajapati Nagar to Lokmanya Nagar

The main features of these corridors along with the details of route alignment have been described below:-

### 4.10.1 Alignment from Automotive Square to KHAPRI

This corridor originates from Automotive Square on Kamptee Road; move along Kamptee Road and reach the intersection point of Amravati Road and Vardha Road, then after crossing Fly Over moves towards Munje Square, moves towards Dhantoli and along nala moves towards Empire/Dr Munje Marg, leads towards Congress Nagar T-Point, then on Rahate Colony Road and then falls on Wardha Road, leads towards NEERI, then moves along Wardha Road and then west of Railway Track in MIHAN area. And passes through 14 m wide stretch of land between the railway boundary line and the road near proposed Container Depot.
There are 17 Statuions proposed on this alignments.

### 4.10.2 Prajapati Nagar to Lokmanya Nagar

This Corridor originates from Prajapati Nagar (meeting point of CA Road and Ring Road), then along Central Avenue Road moves towards Vaishno Devi Chowk, then Mayo Hospita and then takes left turn towards Nagpur Station Entry on Railway Feeder Road, then on Ghat Road alignment takes right turn and crosses over box culvert on existing railway line and falls on State Highway 255, Then after crossing Wardha Road alignment moves along North Ambajharee Road upto Ambajharee Lake and takes left State Highway 255, Then falls on Hingna Road and moves towards Lokmanya Nagar. There are 19 Stations proposed on this alignments.

### 4.10.3 Main features of Alignment from Automotive Square to KHAPRI (North-South Corridor)

Main features of Alignment from Automotive Square to KHAPRlare detailed below:
a) This corridor provides direct metro connectivity to Automotive Square, RBI, Vidhan Sabha, NIT, Zero Mile, Nagpur University, Sitaburdi, Yashvant Stadium, Central Jai, NEERI, Wardha Road, Chhatrapati Shivaji Chowk, Airport, Khapri, MIHAN. Many other prominent places and Government offices are covered in this Corridor.
b) Corridor is integrated with East West corridor at Sitaburdi and this integration provides metro connectivity to new development at Lokmanya Nagar.
c) Corridor integrates with other modes of transport. Bus Terminus near Jhansi Chowk .
d) Entire length ( 19.658 Km .) of this corridor is proposed as elevated except in 4.6 Km at grade after Airport Station and in MIHAN area near Khapri Railway Station.
e) Total 17 stations have been proposed on this corridor; out of these stations 15 stations are elevated and remaining 2 stations are at grade..
f) Future extension of corridor in both directions is feasible.

### 4.10.4 Main features of Alignment from Prajapati Nagar to Lokmanya Nagar (East-West Corridor)

Main features of Alignment from Prajapati Nagar to Lokmanya Nagar are detailed below
a) This corridor provides direct metro connectivity to Central Avenue Road and North Ambajharee Road. This corridor covers many important location like Vardhman Nagar, Mangalwari, Mayo Hospital, Nagpur Railway Station, Santara Market, Sitaburdi, Jhansi Rani Chowk, LAD Square, Ambajharee Lake, Hingna Road, Lokmanya Nagar.
b) Corridor is integrated with North South corridor at Sitaburdi and through that integration prominent location falling on NS Corridor get connected.
c) Corridor integrates with other modes of transport such as Bus Stand near Jhansi Rani Square and Nagpur railway station
d) Entire length of this corridor is proposed as elevated.
e) There are total 19 stations on this corridor and all are elevated.

### 4.11 TECHNICAL FEATURES

4.11.1 Automotive Square to KHAPRI (North-South Corridor)
(a) Horizontal Curves :Horizontal curve details are as per the table below :

Table 4.3: Statement of Horizontal Curves (North-South Corridor)

| Curve No | Direction | Radius | Deflection Angle | Transition Length |  | Tangent | Curve Length | Total Curve Length | Straight between | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | D M S |  |  |  |  |  |  | Start of Alignment -408.17 |
| 1 | Right | 1002.05 | 155353.325 | 25 | 25 | 139.921 | 278.044 | 328.044 | 123.879 |  |
| 2 | Left | 1002.05 | 041534.281 | 25 | 25 | 37.265 | 74.495 | 124.495 | 94.245 |  |
| 3 | Left | 5002.05 | 002708.585 | 15 | 15 | 19.747 | 39.494 | 69.494 | 269.95 |  |
| 4 | Right | 9002.05 | 001127.395 | 15 | 15 | 15 | 30 | 60.000 | 339.022 |  |
| 5 | Right | 3002.05 | 004236.030 | 20 | 20 | 18.601 | 37.201 | 77.201 | 544.771 |  |
| 6 | Left | 3502.05 | 003004.329 | 15 | 15 | 15.317 | 30.635 | 60.635 | 367.154 |  |
| 7 | Left | 1002.05 | 064554.827 | 25 | 25 | 59.228 | 118.318 | 168.318 | 301.632 |  |
| 8 | Right | 232.05 | 061617.226 | 54 | 54 | 12.712 | 25.4 | 133.400 | 86.568 |  |
| 9 | Left | 422.05 | 032624.925 | 50 | 50 | 12.675 | 25.341 | 125.341 | 148.858 |  |
| 10 | Left | 252.05 | 082903.979 | 40 | 40 | 18.696 | 37.324 | 117.324 | 238.516 |  |
| 11 | Right | 1002.05 | 124933.520 | 25 | 25 | 112.628 | 224.314 | 274.314 | 307.758 |  |
| 12 | Left | 1402.05 | 010818.096 | 25 | 25 | 13.929 | 27.856 | 77.856 | 158.651 |  |
| 13 | Left | 202.05 | 080256.113 | 55 | 55 | 14.215 | 28.384 | 138.384 | 87.306 |  |
| 14 | Left | 1002.05 | 130211.452 | 25 | 25 | 114.493 | 227.997 | 277.997 | 27.26 |  |
| 15 | Left | 1502.05 | 011410.942 | 20 | 20 | 16.207 | 32.412 | 72.412 | 138.678 |  |
| 16 | Right | 1602.05 | 005935.134 | 20 | 20 | 13.884 | 27.768 | 67.768 | 412.871 |  |
| 17 | Left | 352.05 | 045214.818 | 50 | 50 | 14.973 | 29.928 | 129.928 | 54.485 |  |
| 18 | Right | 1002.05 | 064035.630 | 25 | 25 | 58.45 | 116.767 | 166.767 | 77.21 |  |
| 19 | Left | 502.05 | 054516.536 | 40 | 40 | 25.233 | 50.424 | 130.424 | 316.656 |  |
| 20 | Left | 182.05 | 270123.322 | 55 | 55 | 43.745 | 85.863 | 195.863 | 27.279 |  |
| 21 | Right | 202.05 | 123559.711 | 40 | 40 | 22.306 | 44.433 | 124.433 | 26.194 |  |
| 22 | Left | 1002.05 | 020631.401 | 25 | 25 | 18.442 | 36.88 | 86.880 | 98.957 |  |
| 23 | Left | 172.05 | 270531.584 | 50 | 50 | 41.452 | 81.353 | 181.353 | 0 |  |
| 24 | Right | 172.05 | 783913.695 | 50 | 50 | 140.956 | 236.185 | 336.185 | 333.31 |  |
| 25 | Left | 1002.05 | 055938.020 | 25 | 25 | 52.462 | 104.828 | 154.828 | 140.502 |  |
| 26 | Right | 162.05 | 661209.831 | 55 | 55 | 105.645 | 187.242 | 297.242 | 121.779 |  |
| 27 | Left | 162.05 | 301535.895 | 55 | 55 | 43.815 | 85.584 | 195.584 | 148.782 |  |

Chapter 04: Geometric Designing Parameters \& Alignment Description

| Curve No | Direction | Radius | Deflection Angle | Transition Length |  | Tangent | Curve Length | Total Curve Length | Straight between | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 28 | Left | 172.05 | 195202.909 | 50 | 50 | 30.132 | 59.659 | 159.659 | 166.886 |  |
| 29 | Right | 1202.05 | 011756.100 | 25 | 25 | 13.626 | 27.251 | 77.251 | 397.271 |  |
| 30 | Right | 6002.05 | 001934.888 | 20 | 20 | 17.094 | 34.188 | 74.188 | 317.309 |  |
| 31 | Left | 1502.05 | 054254.796 | 25 | 25 | 74.976 | 149.829 | 199.829 | 235.665 |  |
| 32 | Left | 552.05 | 024159.255 | 50 | 50 | 13.009 | 26.013 | 126.013 | 0 |  |
| 33 | Right | 522.05 | 024913.936 | 50 | 50 | 12.852 | 25.699 | 125.699 | 579.688 |  |
| 34 | Right | 552.05 | 033642.328 | 50 | 50 | 17.406 | 34.8 | 134.800 | 0 |  |
| 35 | Left | 552.05 | 033151.745 | 50 | 50 | 17.016 | 34.022 | 134.022 | 226.15 |  |
| 36 | Left | 3002.05 | 004818.068 | 20 | 20 | 21.09 | 42.179 | 82.179 | 1733.186 |  |
| 37 | Right | 30002.05 | 000322.518 | 10 | 10 | 14.728 | 29.457 | 49.457 | 435.34 |  |
| 38 | Right | 232.05 | 161034.304 | 55 | 55 | 32.976 | 65.514 | 175.514 | 0 |  |
| 39 | Left | 262.05 | 071141.399 | 55 | 55 | 16.475 | 32.907 | 142.907 | 437.137 |  |
| 40 | Left | 402.05 | 080513.876 | 50 | 50 | 28.421 | 56.749 | 156.749 | 322.908 |  |
| 41 | Right | 402.05 | 091509.718 | 55 | 55 | 32.534 | 64.927 | 174.927 | 125.738 |  |
| 42 | Left | 1002.05 | 030014.782 | 25 | 25 | 26.276 | 52.539 | 102.539 | 313.763 |  |
| 43 | Right | 1002.05 | 015622.429 | 25 | 25 | 16.962 | 33.921 | 83.921 | 169.615 |  |
| 44 | Left | 1502.05 | 011949.060 | 25 | 25 | 17.438 | 34.875 | 84.875 | 476.925 |  |
| 45 | Right | 3002.05 | 003105.547 | 20 | 20 | 13.576 | 27.152 | 67.152 | 436.794 |  |
| 46 | Right | 5002.05 | 003706.348 | 15 | 15 | 26.995 | 53.99 | 83.990 | 409.015 |  |
| 47 | Right | 1002.05 | 062704.991 | 25 | 25 | 56.474 | 112.829 | 162.829 | 112.905 |  |
| 48 | Left | 202.05 | 083029.460 | 45 | 45 | 15.029 | 30.004 | 120.004 | 0 |  |
| 49 | Right | 402.05 | 055536.776 | 40 | 40 | 20.813 | 41.59 | 121.590 | 460.532 |  |
| 50 | Left | 1002.05 | 030209.968 | 25 | 25 | 26.556 | 53.099 | 103.099 | 0 |  |
| 51 | Right | 1002.05 | 033502.177 | 25 | 25 | 31.35 | 62.68 | 112.680 | 591.009 |  |
| 52 | Left | 1002.05 | 044131.197 | 25 | 25 | 41.052 | 82.059 | 132.059 | 467.894 |  |
| 53 | Left | 1002.05 | 023516.664 | 25 | 25 | 22.634 | 45.261 | 95.261 | 101.752 | End of alignment 19250 |


| Abstract of Horizontal Curves( N-S Corridor) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| S. No. | Radius (m) | Nos. <br> Occurrences | Curved <br> Length (m) | \% w. r. t. total curved <br> length |
| 1 | $>160 \mathrm{~m}-200 \mathrm{~m}$ | 9 | 1748.707 | $24.10 \%$ |
| 2 | $>200 \mathrm{~m}-500 \mathrm{~m}$ | 10 | 1408.104 | $19.41 \%$ |
| 3 | $>500 \mathrm{~m}-$ <br> 1000 m | 19 | 2894.656 | $39.89 \%$ |
| 4 | $>1000 \mathrm{~m}-$ <br> 1500 m | 5 | 512.223 | $7.06 \%$ |
| 5 | $>1500 \mathrm{~m}-$ <br> 2000 m | 1 | 67.768 | $0.93 \%$ |
| 6 | $>2000 \mathrm{~m}-$ <br> 5000 m | 6 | 440.651 | $6.07 \%$ |


| 7 | $>5000 m$ | 3 | 183.645 | $2.53 \%$ |
| :---: | :---: | :---: | :---: | :---: |
|  | Total | 53 | 7255.75 | $100.00 \%$ |

## (b) Gradient

A statement showing details of gradients provide along the N S corridor is given in the following Table No. 4.4.

Table 4.4: Statement of Gradients (N-S Corridor)

| S. No. | Chainage |  | Length | Rail Level |  | Gradient | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | From | To |  | From | To |  |  |
| 1 | -408.2 | 300.0 | 708.170 | 303.9 | 303.9 | 0.000\% | Level |
| 2 | 300.0 | 490.0 | 190.000 | 303.9 | 303.5 | -0.211\% | Fall |
| 3 | 490.0 | 840.0 | 350.000 | 303.5 | 308.9 | 1.543\% | Rise |
| 4 | 840.0 | 1110.0 | 270.000 | 308.9 | 308.9 | 0.000\% | Level |
| 5 | 1110.0 | 1410.0 | 300.000 | 308.9 | 309.5 | 0.200\% | Rise |
| 6 | 1410.0 | 1740.0 | 330.000 | 309.5 | 311.5 | 0.606\% | Rise |
| 7 | 1740.0 | 2020.4 | 280.403 | 311.5 | 314.4 | 1.034\% | Rise |
| 8 | 2020.4 | 2270.0 | 249.598 | 314.4 | 314.4 | 0.000\% | Level |
| 9 | 2270.0 | 2460.0 | 190.000 | 314.4 | 310.7 | -1.947\% | Fall |
| 10 | 2460.0 | 2820.0 | 360.000 | 310.7 | 310.1 | -0.167\% | Fall |
| 11 | 2820.0 | 3050.0 | 230.000 | 310.1 | 318.4 | 3.609\% | Rise |
| 12 | 3050.0 | 3312.0 | 262.010 | 318.4 | 318.4 | 0.000\% | Level |
| 13 | 3312.0 | 3680.0 | 367.990 | 318.4 | 318.3 | -0.027\% | Fall |
| 14 | 3680.0 | 3910.0 | 230.000 | 318.3 | 320.9 | 1.130\% | Rise |
| 15 | 3910.0 | 4080.0 | 170.000 | 320.9 | 320.9 | 0.000\% | Level |
| 16 | 4080.0 | 4258.4 | 178.443 | 320.9 | 323.2 | 1.289\% | Rise |
| 17 | 4258.4 | 4550.0 | 291.557 | 323.2 | 323.2 | 0.000\% | Level |
| 18 | 4550.0 | 4756.4 | 206.404 | 323.2 | 322.2 | -0.484\% | Fall |
| 19 | 4756.4 | 5030.0 | 273.596 | 322.2 | 326.3 | 1.499\% | Rise |
| 20 | 5030.0 | 5280.0 | 250.000 | 326.3 | 326.3 | 0.000\% | Level |
| 21 | 5280.0 | 5800.0 | 520.000 | 326.3 | 322.4 | -0.750\% | Fall |
| 22 | 5800.0 | 6050.0 | 250.000 | 322.4 | 319.6 | -1.120\% | Fall |
| 23 | 6050.0 | 6264.0 | 214.000 | 319.6 | 319.6 | 0.000\% | Level |
| 24 | 6264.0 | 6572.8 | 308.756 | 319.6 | 310.9 | -2.818\% | Fall |
| 25 | 6572.8 | 6930.0 | 357.245 | 310.9 | 310.9 | 0.000\% | Level |
| 26 | 6930.0 | 7200.0 | 270.000 | 310.9 | 305.2 | -2.111\% | Fall |
| 27 | 7200.0 | 7400.0 | 200.000 | 305.2 | 310.9 | 2.850\% | Rise |
| 28 | 7400.0 | 7760.0 | 360.000 | 310.9 | 317.9 | 1.944\% | Rise |
| 29 | 7760.0 | 8090.0 | 330.000 | 317.9 | 317.9 | 0.000\% | Level |
| 30 | 8090.0 | 8340.0 | 250.000 | 317.9 | 317.4 | -0.200\% | Fall |
| 31 | 8340.0 | 8530.0 | 190.000 | 317.4 | 321.5 | 2.158\% | Rise |
| 32 | 8530.0 | 8840.0 | 310.000 | 321.5 | 321.5 | 0.000\% | Level |
| 33 | 8840.0 | 9121.7 | 281.737 | 321.5 | 322.4 | 0.319\% | Rise |
| 34 | 9121.7 | 9340.0 | 218.263 | 322.4 | 320 | -1.100\% | Fall |
| 35 | 9340.0 | 9680.0 | 340.000 | 320 | 316.1 | -1.147\% | Fall |
| 36 | 9680.0 | 9900.0 | 220.000 | 316.1 | 315.3 | -0.364\% | Fall |
| 37 | 9900.0 | 10205.0 | 305.000 | 315.3 | 315.3 | 0.000\% | Level |


| S. No. | Chainage |  | Length | Rail Level |  | Gradient | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | From | To |  | From | To |  |  |
| 38 | 10205.0 | 10730.0 | 525.000 | 315.3 | 319.5 | $0.800 \%$ | Rise |
| 39 | 10730.0 | 11283.4 | 553.428 | 319.5 | 319.5 | $0.000 \%$ | Level |
| 40 | 11283.4 | 11670.0 | 386.572 | 319.5 | 320 | $0.129 \%$ | Rise |
| 41 | 11670.0 | 11930.0 | 260.000 | 320 | 320 | $0.000 \%$ | Level |
| 42 | 11930.0 | 12560.0 | 630.000 | 320 | 311 | $-1.429 \%$ | Fall |
| 43 | 12560.0 | 12960.0 | 400.000 | 311 | 311 | $0.000 \%$ | Level |
| 44 | 12960.0 | 13100.0 | 140.000 | 311 | 307.1 | $-2.786 \%$ | Fall |
| 45 | 13100.0 | 13360.0 | 260.000 | 307.1 | 307.5 | $0.154 \%$ | Rise |
| 46 | 13360.0 | 13680.0 | 320.000 | 307.5 | 313.3 | $1.813 \%$ | Rise |
| 47 | 13680.0 | 14098.9 | 418.920 | 313.3 | 313.3 | $0.000 \%$ | Level |
| 48 | 14098.9 | 14370.0 | 271.080 | 313.3 | 307.6 | $-2.103 \%$ | Fall |
| 49 | 14370.0 | 14720.0 | 350.000 | 307.6 | 304.8 | $-0.800 \%$ | Fall |
| 50 | 14720.0 | 15500.0 | 780.000 | 304.8 | 295.6 | $-1.179 \%$ | Fall |
| 51 | 15500.0 | 15700.0 | 200.000 | 295.6 | 295.6 | $0.000 \%$ | Level |
| 52 | 15700.0 | 16080.0 | 380.000 | 295.6 | 299 | $0.895 \%$ | Rise |
| 53 | 16080.0 | 16330.0 | 250.000 | 299 | 299 | $0.000 \%$ | Level |
| 54 | 16330.0 | 17080.0 | 750.000 | 299 | 307.6 | $1.147 \%$ | Rise |
| 55 | 17080.0 | 17324.6 | 244.621 | 307.6 | 316 | $3.434 \%$ | Rise |
| 56 | 17324.6 | 17550.0 | 225.379 | 316 | 316 | $0.000 \%$ | Level |
| 57 | 17550.0 | 17740.0 | 190.000 | 316 | 308.5 | $-3.947 \%$ | Fall |
| 58 | 17740.0 | 18020.0 | 280.000 | 308.5 | 310.7 | $0.786 \%$ | Rise |
| 59 | 18020.0 | 18232.0 | 212.000 | 310.7 | 308.7 | $-0.943 \%$ | Fall |
| 60 | 18232.0 | 18610.1 | 378.100 | 308.7 | 308.7 | $0.000 \%$ | Level |
| 61 | 18610.1 | 19250.0 | 639.900 | 308.7 | 302.5 | $-0.969 \%$ | Fall |
| 62 | 19250.0 | 20357.2 | 1107.242 | 302.5 | 292 | $-0.948 \%$ | Fall |


| Abstract of Gradients( N-S Corridor) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| S. <br> No. | Description | Nos. <br> Occurrences | Length (m) | \% w. r. t. total <br> Alignment <br> length |
| 1 | Level | 20 | 5233.013 | $26.62 \%$ |
| 2 | $>0 \%$ to $=1 \%$ | 22 | 9040.247 | $45.99 \%$ |
| 3 | $>1 \%$ to $=2 \%$ | 11 | 3340.303 | $16.99 \%$ |
| 4 | $>2 \%$ to $=3 \%$ | 5 | 1108.756 | $5.64 \%$ |
| 5 | $>3 \%$ to $=4 \%$ | 4 | 935.701 | $4.76 \%$ |
|  | Total | 62 | 19658.2 | $100.00 \%$ |

### 4.11.2 Prajapati Nagar to Lokmanya Nagar (East-West Corridor)

(a) Horizontal Curves:The details of horizontal curves is shown in Table 4.5:

Table 4.5: Statement of Horizontal Curves (East-West Corridor)

Table 4.5

| Curve <br> No | Direc- <br> tion | Radius | Deflection <br> Angle | Transition <br> Length |  | Tangent | Curve <br> Length | Total <br> Curve <br> Length | Straight <br> between |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | D M S |  |  |  |  |  | 66.102 |
| 1 | Right | 202.05 | 371046.630 | 55 | 55 | 67.957 | 131.112 | 241.112 | 172.073 |
|  |  |  |  |  |  | Remarks <br> Alignment <br> -392 |  |  |  |
| 2 | Right | 402.05 | 284253.968 | 50 | 50 | 102.911 | 201.496 | 301.496 | 217.679 |


| $\begin{array}{c}\text { Curve } \\ \text { No }\end{array}$ | $\begin{array}{c}\text { Direc- } \\ \text { tion }\end{array}$ | Radius | $\begin{array}{c}\text { Deflection } \\ \text { Angle }\end{array}$ | $\begin{array}{c}\text { Transition } \\ \text { Length }\end{array}$ |  | Tangent | $\begin{array}{c}\text { Curve } \\ \text { Length }\end{array}$ | $\begin{array}{c}\text { Total } \\ \text { Curve } \\ \text { Length }\end{array}$ | $\begin{array}{c}\text { Straight } \\ \text { between }\end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 36 | Left | 172.05 | 733835.753 | 56 | 56 | 128.811 | 221.139 | 333.139 | 490.256 |
| 37 | Right | 182.05 | 114730.843 | 55 | 55 | 18.8 | 37.467 | 147.467 | 28.414 |
| 38 | Right | 162.05 | 311655.272 | 55 | 55 | 45.37 | 88.475 | 198.475 | 224.703 |
| 39 | Left | 222.05 | 000256.634 | 50 | 50 | 0.095 | 0.19 | 100.19 | 317.926 |
| 40 | Left | 15002.05 | 000751.774 | 15 | 15 | 17.157 | 34.313 | 64.313 | 360.846 |
| 41 | Left | 9502.05 | 000905.222 | 15 | 15 | 12.558 | 25.117 | 55.117 | 877.118 |
| 42 | Left | 402.05 | 074336.044 | 50 | 50 | 27.151 | 54.219 | 154.219 | 500.994 |
| 43 | Right | 202.05 | 131212.862 | 55 | 55 | 23.384 | 46.562 | 156.562 | 56.253 |
| 44 | Left | 202.05 | 252308.620 | 55 | 55 | 45.507 | 89.521 | 199.521 | 359.319 |$]$


| Abstract of Horizontal Curves( E-W Corridor) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| S. <br> No. | Radius (m) | Nos. <br> Occurrences | Curved <br> Length (m) | \% w.r.t. total <br> curved length |
| 1 | $>160 \mathrm{~m}-200 \mathrm{~m}$ | 3 | 679.081 | $10.64 \%$ |
| 2 | $>200 \mathrm{~m}-500 \mathrm{~m}$ | 17 | 2918.441 | $45.72 \%$ |
| 3 | $>500 \mathrm{~m}-$ <br> 1000 m | 13 | 1453.44 | $22.77 \%$ |
| 4 | $>1000 \mathrm{~m}-$ <br> 1500 m | 5 | 726.731 | $11.39 \%$ |
| 5 | $>1500 \mathrm{~m}-$ <br> 2000 m | 2 | 129.172 | $2.02 \%$ |
| 6 | $>200 \mathrm{~m}-$ <br> 5000 m | 1 | 119.007 | $1.86 \%$ |
| 7 | $>5000 \mathrm{~m}$ | 6 | 357.356 | $5.60 \%$ |

(c) Gradient

A statement showing details of gradients provide along the corridor is given in the following Table No. 4.6: -

Table 4.6: Statement of Gradients (East-West Corridor)

| S. <br> No. | Chainage |  | Length | Rail Level |  | Gradient | Remarks |
| :---: | :---: | :---: | :--- | ---: | ---: | :---: | :---: |
|  | From | To |  | From | To |  |  |
| 1 | -392.00 | 180.00 | 572.000 | 301 | 301 | $0.000 \%$ | Level |
| 2 | 180.00 | 430.00 | 250.000 | 301 | 297.2 | $-1.520 \%$ | Fall |
| 3 | 430.00 | 700.00 | 270.000 | 297.2 | 300.5 | $1.222 \%$ | Rise |
| 4 | 700.00 | 1087.35 | 387.348 | 300.5 | 305.3 | $1.239 \%$ | Rise |


| $\begin{gathered} \text { S. } \\ \text { No. } \end{gathered}$ | Chainage |  | Length | Rail Level |  | Gradient | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | From | To |  | From | To |  |  |
| 5 | 1087.35 | 1320.00 | 232.652 | 305.3 | 305.3 | 0.000\% | Level |
| 6 | 1320.00 | 1570.00 | 250.000 | 305.3 | 304.6 | -0.280\% | Fall |
| 7 | 1570.00 | 1820.80 | 250.800 | 304.6 | 308.3 | 1.475\% | Rise |
| 8 | 1820.80 | 2078.76 | 257.955 | 308.3 | 308.3 | 0.000\% | Level |
| 9 | 2078.76 | 2440.00 | 361.245 | 308.3 | 308.9 | 0.166\% | Rise |
| 10 | 2440.00 | 2640.00 | 200.000 | 308.9 | 309.7 | 0.400\% | Rise |
| 11 | 2640.00 | 3020.00 | 380.000 | 309.7 | 311.6 | 0.500\% | Rise |
| 12 | 3020.00 | 3235.00 | 215.000 | 311.6 | 311.6 | 0.000\% | Level |
| 13 | 3235.00 | 3384.00 | 149.000 | 311.6 | 310.9 | -0.470\% | Fall |
| 14 | 3384.00 | 3772.20 | 388.200 | 310.9 | 311.5 | 0.155\% | Rise |
| 15 | 3772.20 | 4180.00 | 407.800 | 311.5 | 311.5 | 0.000\% | Level |
| 16 | 4180.00 | 4340.00 | 160.000 | 311.5 | 311 | -0.313\% | Fall |
| 17 | 4340.00 | 4652.53 | 312.525 | 311 | 319.5 | 2.720\% | Rise |
| 18 | 4652.53 | 4922.00 | 269.475 | 319.5 | 319.5 | 0.000\% | Level |
| 19 | 4922.00 | 5190.00 | 268.000 | 319.5 | 316.7 | -1.045\% | Fall |
| 20 | 5190.00 | 5490.00 | 300.000 | 316.7 | 321.9 | 1.733\% | Rise |
| 21 | 5490.00 | 5750.00 | 260.000 | 321.9 | 321.9 | 0.000\% | Level |
| 22 | 5750.00 | 5940.00 | 190.000 | 321.9 | 325.5 | 1.895\% | Rise |
| 23 | 5940.00 | 6350.00 | 410.000 | 325.5 | 319.7 | -1.415\% | Fall |
| 24 | 6350.00 | 6580.00 | 230.000 | 319.7 | 319.7 | 0.000\% | Level |
| 25 | 6580.00 | 6890.00 | 310.000 | 319.7 | 313.1 | -2.129\% | Fall |
| 26 | 6890.00 | 7130.00 | 240.000 | 313.1 | 313.1 | 0.000\% | Level |
| 27 | 7130.00 | 7290.00 | 160.000 | 313.1 | 310.2 | -1.813\% | Fall |
| 28 | 7290.00 | 7615.00 | 325.000 | 310.2 | 320.1 | 3.046\% | Rise |
| 29 | 7615.00 | 7856.99 | 241.990 | 320.1 | 320.1 | 0.000\% | Level |
| 30 | 7856.99 | 8200.00 | 343.010 | 320.1 | 313.9 | -1.808\% | Fall |
| 31 | 8200.00 | 8523.50 | 323.499 | 313.9 | 313.9 | 0.000\% | Level |
| 32 | 8523.50 | 8770.00 | 246.502 | 313.9 | 311.6 | -0.933\% | Fall |
| 33 | 8770.00 | 8965.00 | 195.000 | 311.6 | 315.4 | 1.949\% | Rise |
| 34 | 8965.00 | 9241.43 | 276.433 | 315.4 | 315.4 | 0.000\% | Level |
| 35 | 9241.43 | 9490.00 | 248.567 | 315.4 | 312.6 | -1.126\% | Fall |
| 36 | 9490.00 | 9770.00 | 280.000 | 312.6 | 313.3 | 0.250\% | Rise |
| 37 | 9770.00 | 9965.00 | 195.000 | 313.3 | 316.9 | 1.846\% | Rise |
| 38 | 9965.00 | 10190.00 | 225.000 | 316.9 | 316.9 | 0.000\% | Level |
| 39 | 10190.00 | 10500.00 | 310.000 | 316.9 | 314.8 | -0.677\% | Fall |
| 40 | 10500.00 | 10765.00 | 265.000 | 314.8 | 319.1 | 1.623\% | Rise |


| $\begin{aligned} & \text { S. } \\ & \text { No. } \end{aligned}$ | Chainage |  | Length | Rail Level |  | Gradient | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | From | To |  | From | To |  |  |
| 41 | 10765.00 | 10990.00 | 225.000 | 319.1 | 319.1 | 0.000\% | Level |
| 42 | 10990.00 | 11360.00 | 370.000 | 319.1 | 318.8 | -0.081\% | Fall |
| 43 | 11360.00 | 11845.00 | 485.000 | 318.8 | 329.5 | 2.206\% | Rise |
| 44 | 11845.00 | 12130.00 | 285.000 | 329.5 | 329.5 | 0.000\% | Level |
| 45 | 12130.00 | 12370.00 | 240.000 | 329.5 | 325 | -1.875\% | Fall |
| 46 | 12370.00 | 12710.00 | 340.000 | 325 | 336 | 3.235\% | Rise |
| 47 | 12710.00 | 13160.00 | 450.000 | 336 | 336 | 0.000\% | Level |
| 48 | 13160.00 | 13550.00 | 390.000 | 336 | 333.2 | -0.718\% | Fall |
| 49 | 13550.00 | 14060.00 | 510.000 | 333.2 | 338.8 | 1.098\% | Rise |
| 50 | 14060.00 | 14300.00 | 240.000 | 338.8 | 338.8 | 0.000\% | Level |
| 51 | 14300.00 | 14580.00 | 280.000 | 338.8 | 339.4 | 0.214\% | Fall |
| 52 | 14580.00 | 14875.00 | 295.000 | 339.4 | 340.4 | 0.339\% | Rise |
| 53 | 14875.00 | 15050.00 | 175.000 | 340.4 | 345.2 | 2.743\% | Rise |
| 54 | 15050.00 | 15270.00 | 220.000 | 345.2 | 345.2 | 0.000\% | Level |
| 55 | 15270.00 | 15532.00 | 262.000 | 345.2 | 342.5 | -1.031\% | Fall |
| 56 | 15532.00 | 15770.00 | 238.000 | 342.5 | 339.2 | -1.387\% | Fall |
| 57 | 15770.00 | 16020.00 | 250.000 | 339.2 | 336.3 | -1.160\% | Fall |
| 58 | 16020.00 | 16289.74 | 269.742 | 336.3 | 336.3 | 0.000\% | Level |
| 59 | 16289.74 | 16500.00 | 210.258 | 336.3 | 332.4 | -1.855\% | Fall |
| 60 | 16500.00 | 16800.00 | 300.000 | 332.4 | 332.2 | -0.067\% | Fall |
| 61 | 16800.00 | 16960.00 | 160.000 | 332.2 | 333.3 | 0.688\% | Rise |
| 62 | 16960.00 | 17160.00 | 200.000 | 333.3 | 330.4 | -1.450\% | Fall |
| 63 | 17160.00 | 17496.76 | 336.758 | 330.4 | 330.4 | 0.000\% | Level |


| Abstract of Gradients( E-W Corridor) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| S. No. | Description | Nos. <br> Occurrences | Length (m) | \% w.r.t. total <br> Alignment <br> length |
| 1 | Level | 20 | 6054.412 | $33.33 \%$ |
| 2 | $>0 \%$ to $=1 \%$ | 16 | 4519.947 | $24.88 \%$ |
| 3 | $>1 \%$ to $=2 \%$ | 21 | 5642.983 | $31.07 \%$ |
| 4 | $>2 \%$ to $=3 \%$ | 4 | 1282.525 | $7.06 \%$ |
| 5 | $>3 \%$ to $=4 \%$ | 2 | 665 | $3.66 \%$ |
|  | Total | $\mathbf{6 3}$ | $\mathbf{1 8 1 6 5}$ | $100.00 \%$ |

